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# Air Force Research Laboratory



***Integrity ★ Service ★ Excellence***

## Hydrolytic Network Structure Degradation in Multi-Component Polycyanurate Networks

28 July 2016

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# Outline



- **Background**
- **Quantitative Models**
- **New Data**



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- **Air Force Research Laboratory, Rocket Propulsion Division**
- **Air Force Office of Scientific Research**
- **Mr. Jason Lamb, optical microscopy**
- **Mr. Michael Ford, chemistry support**



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# Cyanate Esters for Next-Generation Aerospace Systems



Glass Transition Temperature  
200 – 400 °C (dry)  
150 – 300 °C (wet)

Resin Viscosity  
Suitable for  
Filament  
Winding / RTM

Compatible with  
Thermoplastic  
Tougheners and  
Nanoscale  
Reinforcements

High  $T_g$

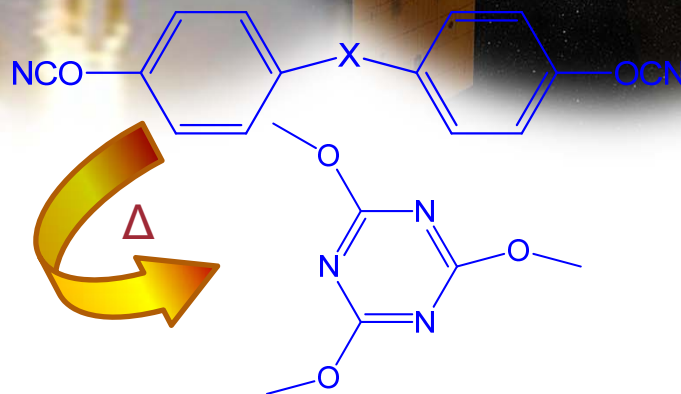
Onset of Weight  
Loss:  
> 400 °C with High  
Char Yield

Ease of  
Processing

Resistance to  
Harsh  
Environments

Good Flame,  
Smoke, &  
Toxicity  
Characteristics

Low Water Uptake  
with Near Zero  
Coefficient of  
Hygroscopic  
Expansion







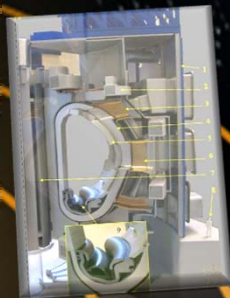
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# Cyanate Esters Around the Solar System



## Our Solar System

- On Earth, cyanate ester / epoxy blends have been qualified for use in the toroidal field magnet casings for the ITER thermonuclear fusion reactor



Fusion reactor, photo courtesy of Gerritse ((Wikimedia Commons))

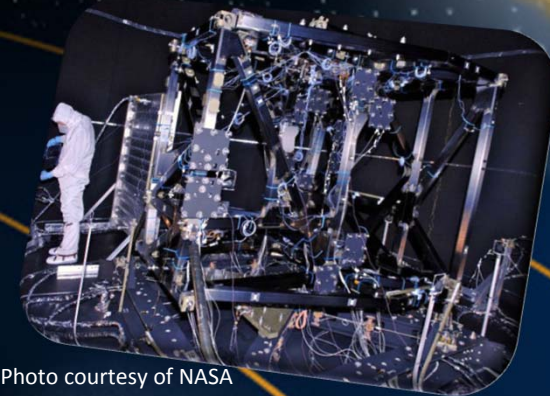


Photo courtesy of NASA

- Unique cyanate ester composites have been designed by NASA for use as instrument holding structures aboard the James Webb Space Telescope
- The science decks on the Mars Phoenix lander are made from M55J/cyanate ester composites
- The solar panel supports on the MESSENGER space probe use cyanate ester composite tie layers

Images: courtesy NASA (public release)



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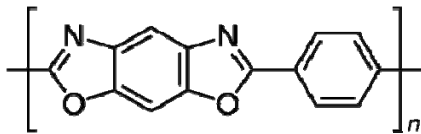
# Importance of Moisture Uptake in Composite Component Performance



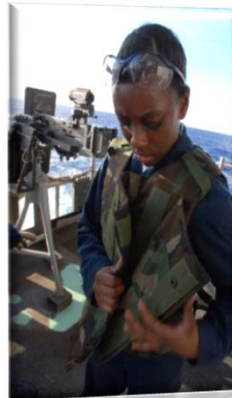
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- Water can add significantly to launch or take-off weight (3% water in composite resins = about 50 lbs of extra weight on an large SRM)
- Items with high water content can fail catastrophically when suddenly heated
- Long-term exposure to water can facilitate many mechanisms of chemical degradation, necessitating substantial “knock down” factors in design allowables
- Though more stable than epoxy resins, cyanate esters can degrade on long-term exposure to hot water



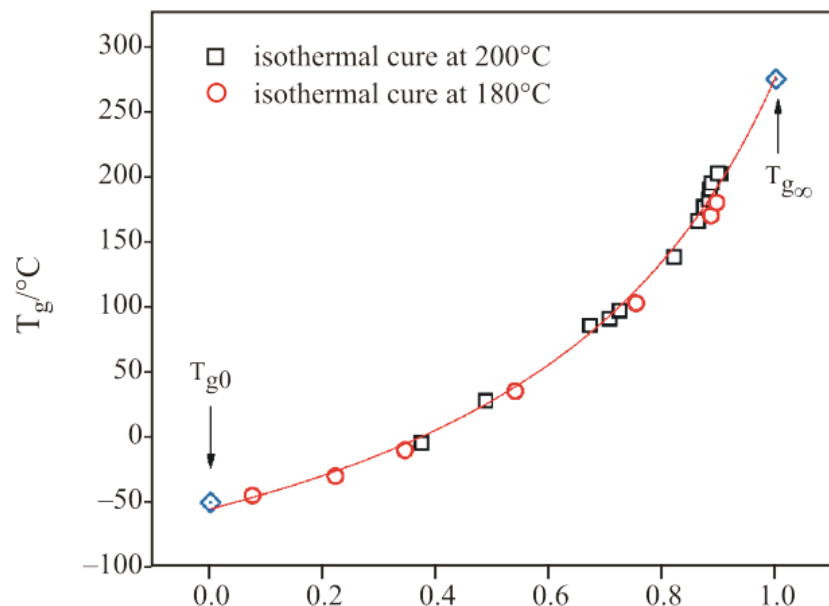




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# Models for Network Initial States



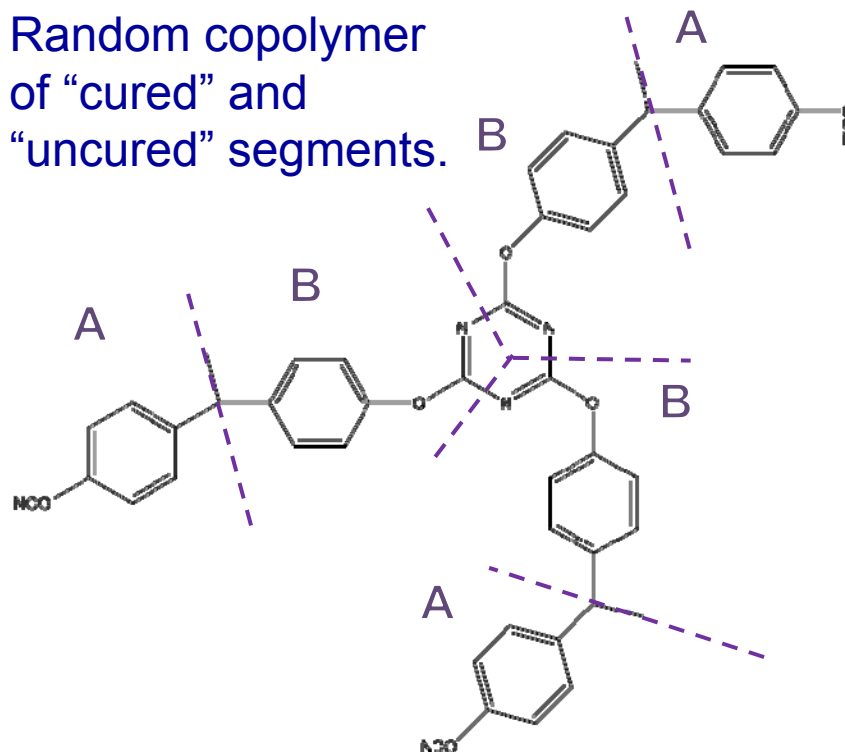
from X. Sheng, M. Akinc, and M. R. Kessler, *J. Therm. Anal. Calorim.* **2008**, 93, 77-85 for EX-1510

DiBenedetto equation is just Gordon-Taylor equation recast with  $1-\alpha = \phi_1$ ,  $\lambda = k$

## Assumptions:

$\Delta H_{mix} = 0$ ;  $\Delta S_{mix} = 0$ ,  $\Delta v_{mix} = 0$ ,  
S continuous at  $T_G$ ,  $dS/dP = 0$

Random copolymer of “cured” and “uncured” segments.



No volume change on cure, so  $\alpha = \phi_{cured}$

## Consequence

Initial state of network entirely described by one parameter -  $\alpha$

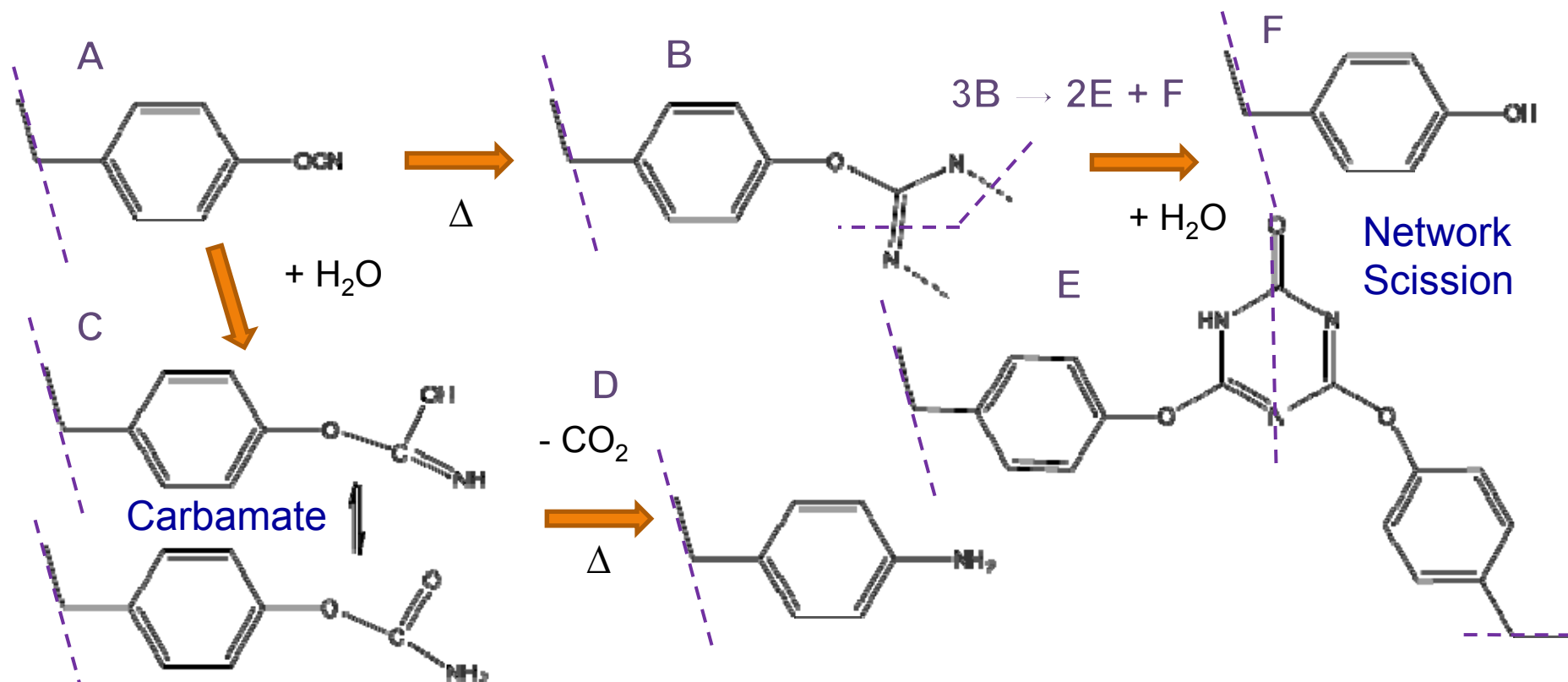




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# Chemical Reaction Scheme



Network states:

$\phi_A, \dots, \phi_F$   $\phi_E$  and  $\phi_F$  related by stoichiometry

If networks are heated only to 350 °C, then only one of  $\phi_C$  or  $\phi_D$  may be non-zero.

Result: three parameters prior to heating: network conversion  $\alpha'$  based on  $\phi_B$ , plus  $\phi_C$  and  $\phi_F$ . Two parameters after heating,  $\phi_D$  and  $\phi_F$ .



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# Chemical Reaction Models

## Carbamate formation



Weight gain of  $0.14\phi_c$

Loss of  $\Delta H_{\text{cure}}$ , Loss of FT-IR signal at  $2250 \text{ cm}^{-1}$ , gain in FT-IR signal at  $1700 \text{ cm}^{-1}$ , no change in  $T_G$

## Carbamate decomposition



Heating to  $350^\circ\text{C}$  will complete

Weight loss of  $0.34\phi_c$

No change in  $\Delta H_{\text{cure}}$ , Loss of FT-IR signal at  $17000 \text{ cm}^{-1}$ , no change in  $T_G$

## Other decomposition



*Assumed negligible below  $350^\circ\text{C}$*

## Residual Cure



Heating to  $350^\circ\text{C}$  dry will complete

No weight change

Loss of  $\Delta H_{\text{cure}}$ , Loss of FT-IR signal at  $2250 \text{ cm}^{-1}$ , increase in  $T_G$

## Network Scission



Weight gain of  $0.14\phi_E$

No change in  $\Delta H_{\text{cure}}$ , only discernible readily via near-IR, decrease in  $T_G$

### More details:

Davis, M. C.; Guenther, A. J.; Sahagun, C. M.; Lamison, K. R.; Reams, J. T.; Mabry, J. M. "*Polymer* **2013**, *54*, 6902-6909.

Marella, V. V.; Throckmorton, J. A.; Palmese, G. R. *Polym. Degrad. Stabil.* **2014**, *104*, 104-111.



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# Effective Conversion Reduction

Multi-Component Gordon-Taylor Equation:

$$T_G = (T_{GA} \phi_A + k_{BA} T_{GB} \phi_B + \dots + k_{EA} T_{GF} \phi_F) / (\phi_A + k_{BA} \phi_B + \dots + k_{FA} \phi_F)$$

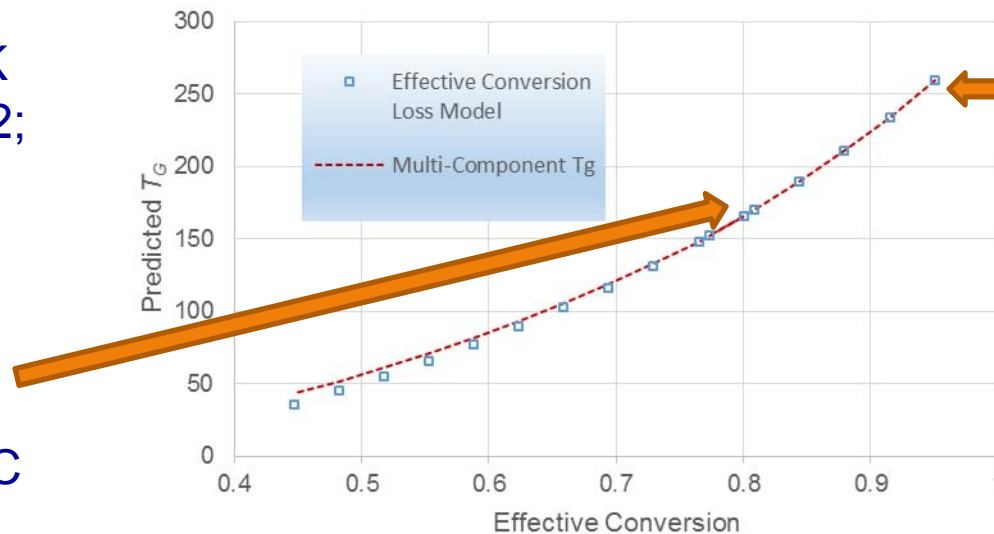
Can be simplified using an “effective conversion reduction factor”  $K$

$$\alpha'_{eff} = \alpha'_0 - K\phi_F$$

$$T_G = T_{G0} + (T_{G\infty} - T_{G0}) \lambda \alpha'_{eff} / [1 - (1-\lambda) \alpha'_{eff}] \quad (\text{just the diBenedetto equation})$$

Assumes:  
Same network  
physics  
throughout  
hydrolysis;  $\phi_C$   
and  $\phi_F$   
are correlated

Test 1: Use  $K$   
from  $\phi_F = 0.02$ ;  
(Test 1)  
extrapolate to  
 $\phi_F = 0.2$  with  
 $\alpha'_0 = 0.8$  and  
 $\phi_C / \phi_F = 1$ ;  
Max error 8 °C



Test 1: Use  $K$   
from  $\phi_F = 0.02$ ;  
 $\alpha'_0 = 0.95$ ,  
 $\phi_C / \phi_F = 0.5$ ;  
extrapolate to  
 $\phi_F = 0.1$ . Max  
error 1 °C

Test Parameters;  $k_{BA} = 0.4$ ;  $T_{GB} = 300$  °C;  $k_{CA} = 1.2$ ;  $T_{GC} = 0$  °C;  $k_{DA} = 0.9$ ;  $T_{GD} = -30$  °C;  $k_{EA} = 0.6$ ;  $T_{GE} = 100$  °C;  $k_{FA} = 0.8$ ;  $T_{GF} = -20$  °C;

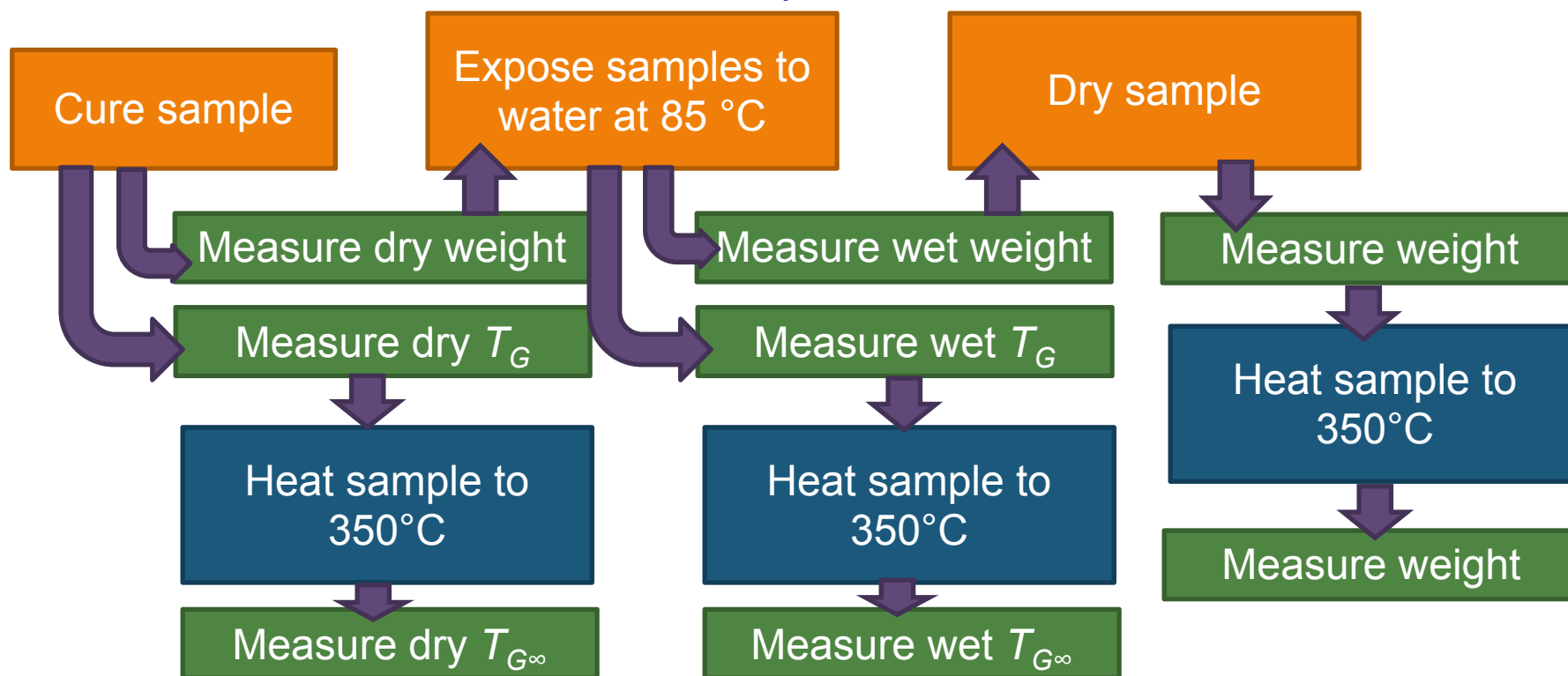


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# Analysis Procedure

Assumes diBenedetto parameters are known



FT-IR may be added for verification if possible. Dry sample glass transition best if measured by DSC; wet glass transition best if measured by TMA

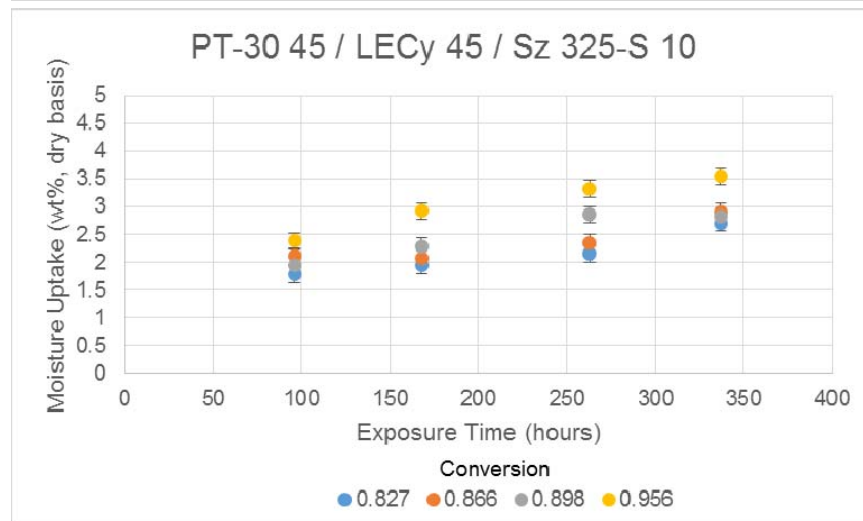
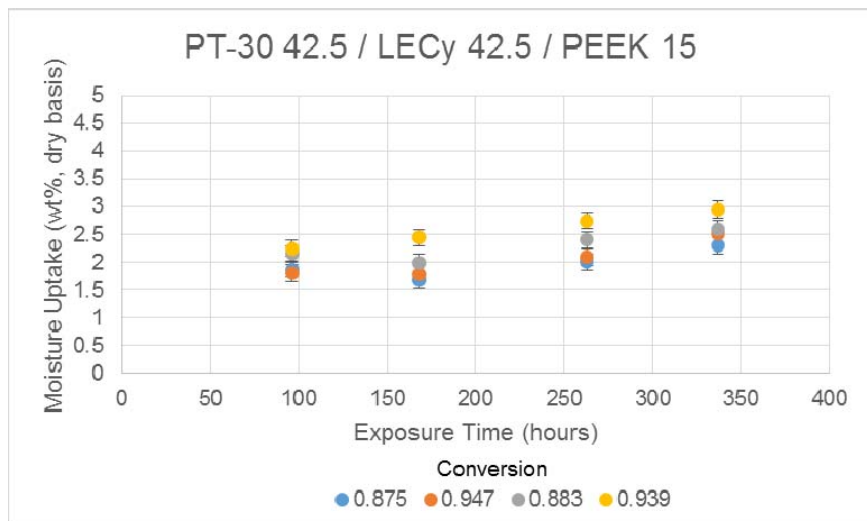
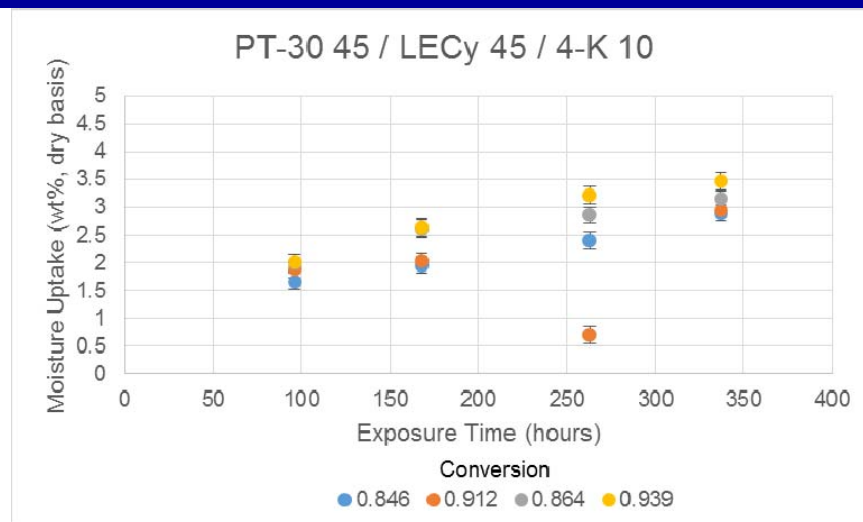
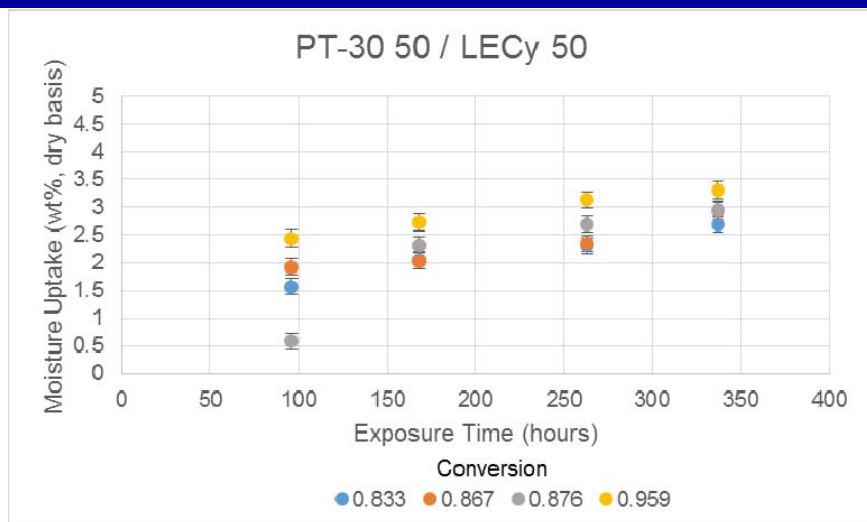
Final “wet and dried” weights determine –  $\phi_C$ ,  $\phi_F$ .  $T_{G\infty}$  data cross-checks other degradation.





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# Weight Gain After Water Exposure (No Drying)

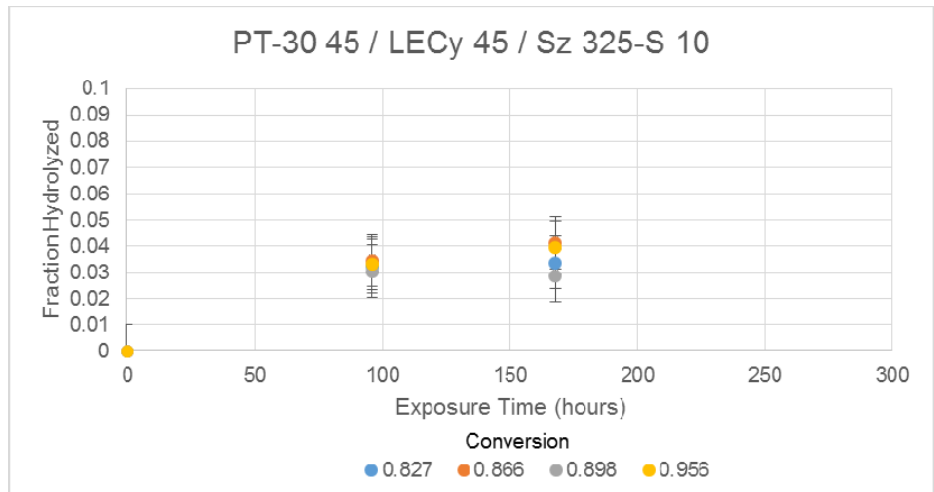
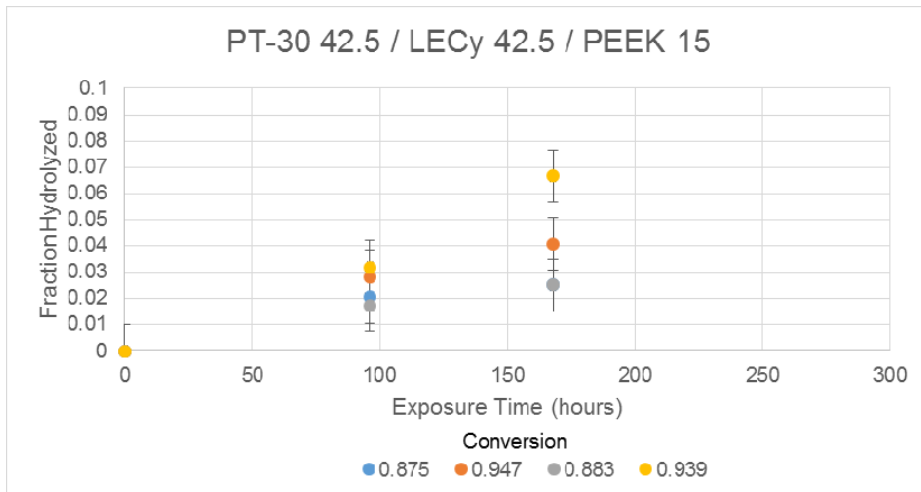
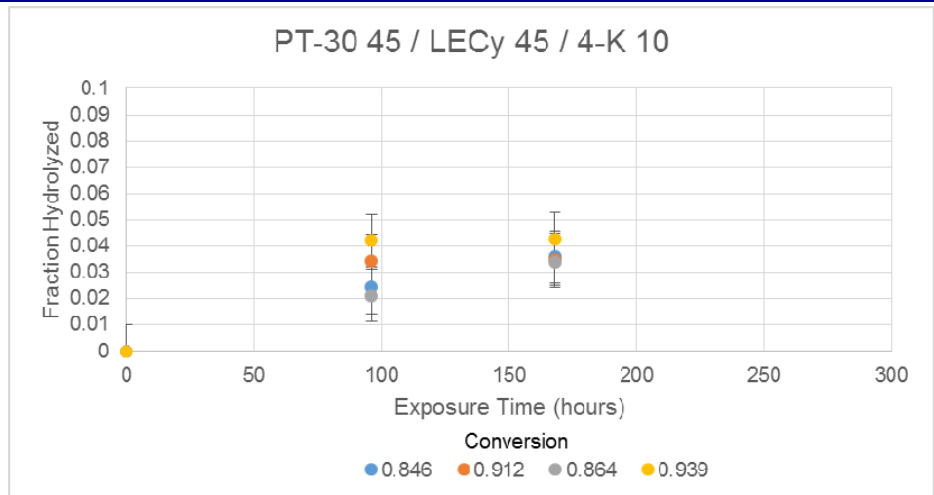
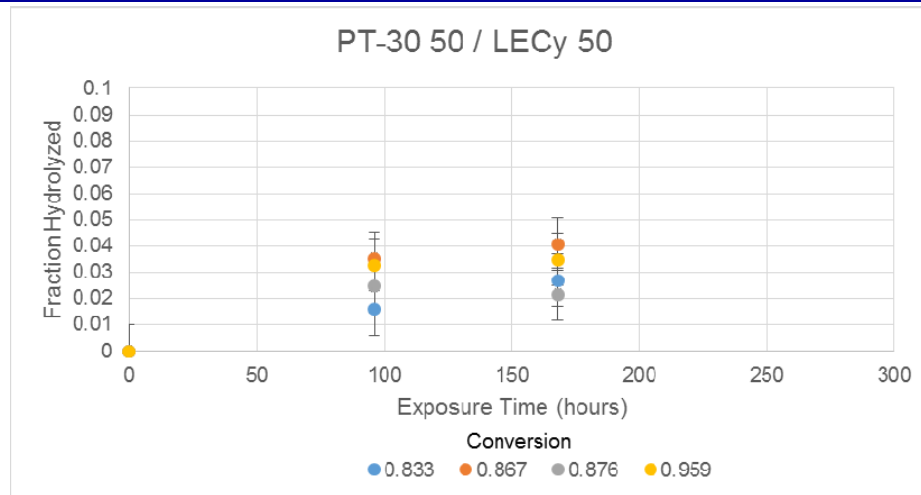


Slow hydrolysis evident; conversion dependence as expected  
PEEK reduces water uptake as expected



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# Hydrolysis Extent After Water Exposure



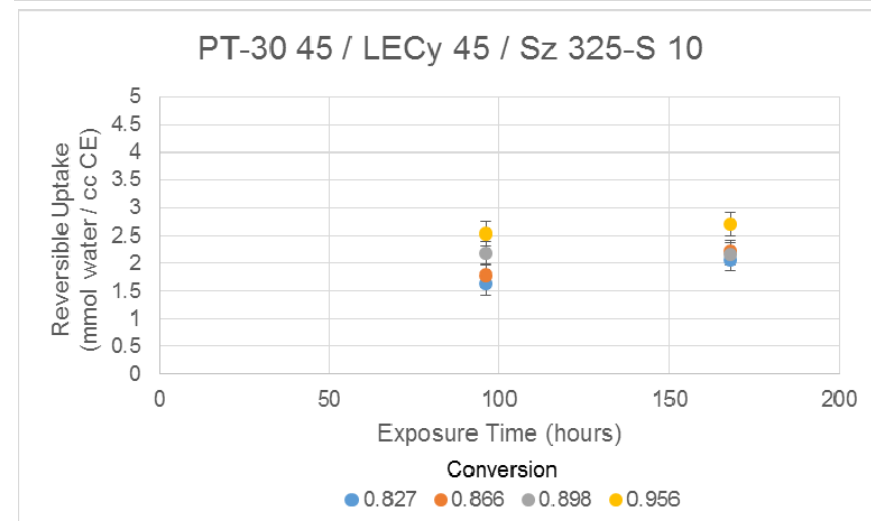
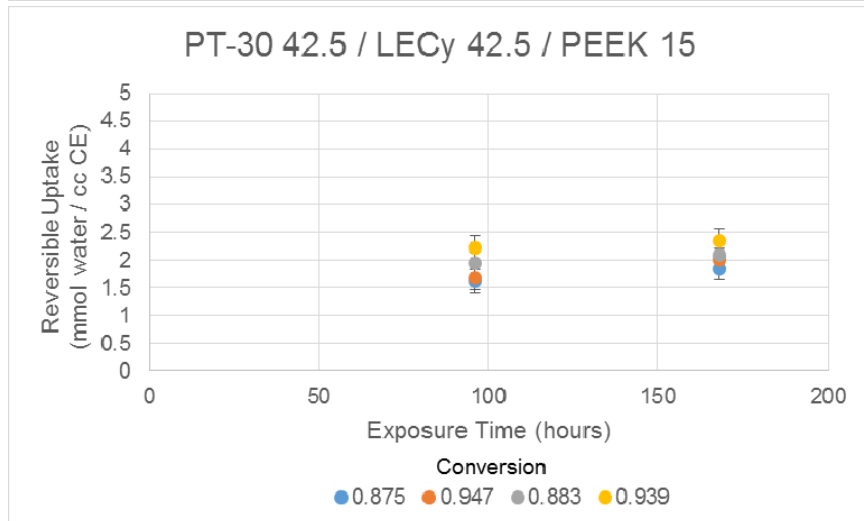
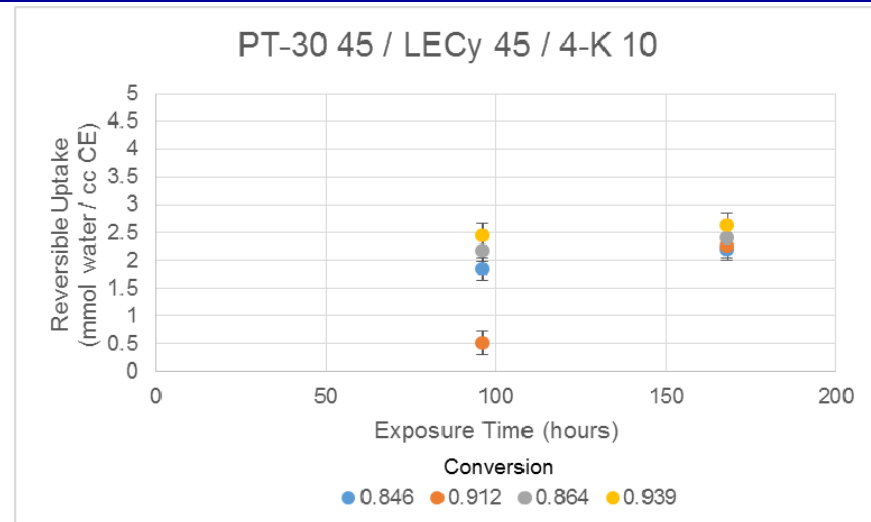
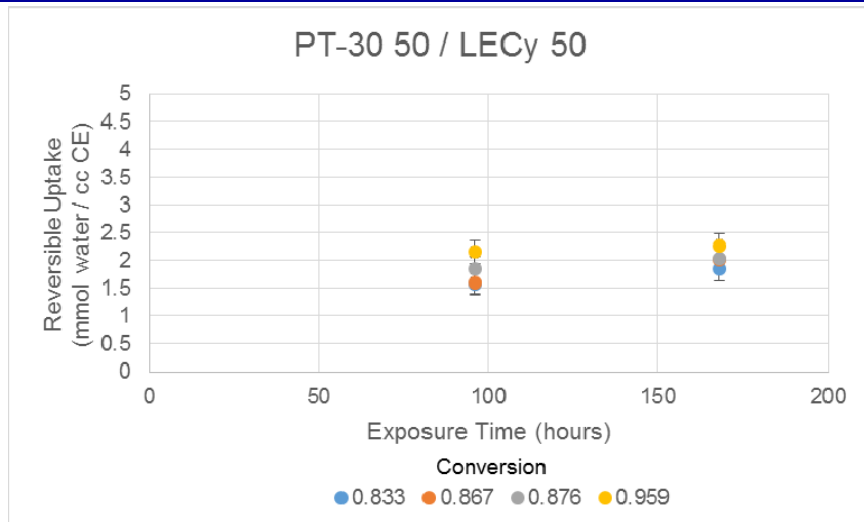
Data from samples exposed and dried with mild heating; slight correlation with conversion; additives show little effect so far ...



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# Estimated Water Concentration



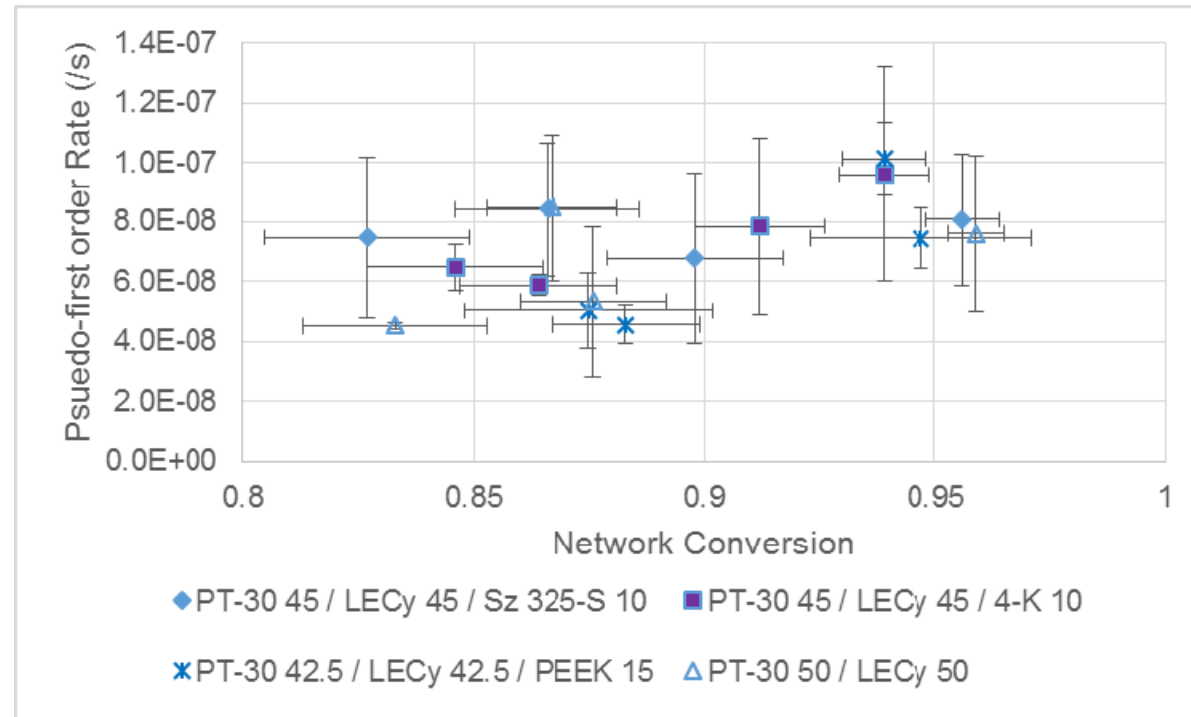
Mica appears to add water and inhibit diffusion. Diffusion appears to be faster at higher conversions.



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# Preliminary Kinetic Data



Conversions are from DSC only and are preliminary

Rate constant is for all hydrolysis reactions – includes carbamate formation and network scission

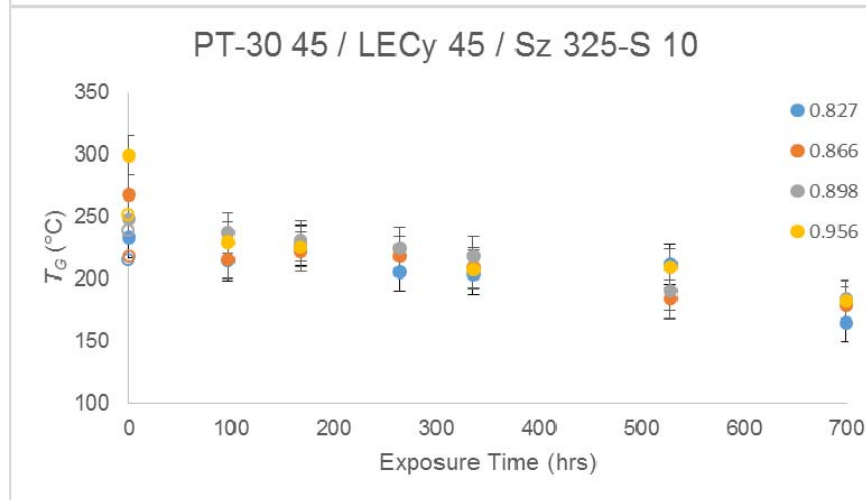
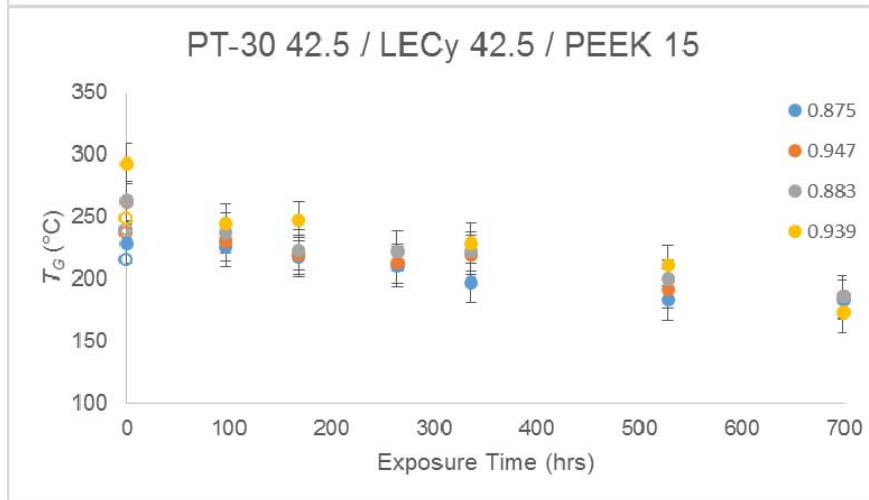
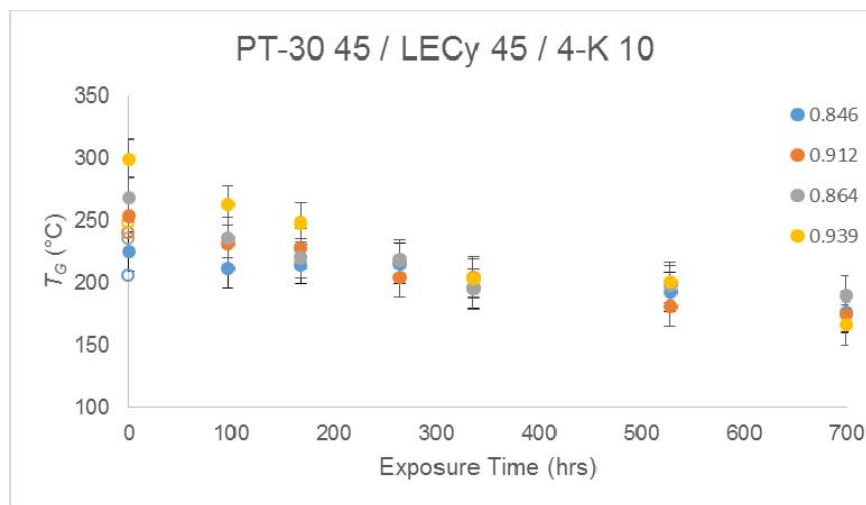
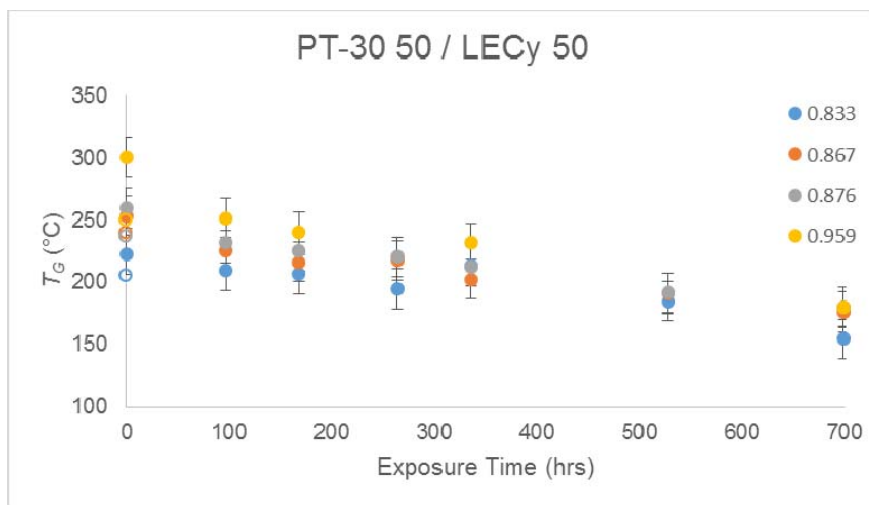




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# Glass Transition Temperature



DSC data for dry samples is shown as open symbols; in-situ cure affects results at early times, even after exposure, proving –OCN groups are still present



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# Summary



- The relative simplicity of the chemical structure of polycyanurate networks, in combination with ease of analysis, allows for quantitative modeling of hydrolytic degradation. These models link chemical structure, physical properties, and environmental conditions, while allowing for validation.
- Hydrolytic degradation processes have been quantified for Cu/nonylphenol-catalyzed, co-cured LECy/PT-30 networks, with and without additives for toughening, under exposure to hot water. The effects of conversion have been examined.
- Preliminary data shows rates of hydrolysis that are lower than for PT-30 alone. Overall hydrolysis rates appear to be slightly higher at higher conversions, suggesting that carbamate formation is not responsible for a large portion of weight gain.
- Glass transition temperatures decrease gradually as expected. Determination of the effective network conversion reduction parameter requires further work to distinguish carbamate formation from network scission.

